Control of Series Resonant Converter with Robust Performance Against Load and Power Circuit Components Uncertainties

A. Mohammadpour*, H. Mokhtari* and M. R. Zolghadri*

Abstract: Robust performance controller design for duty-cycle controlled series resonant converter (SRC) is proposed in this paper. The uncertainties of the converter are analyzed with load variation and power circuit components tolerances are taken into consideration. Additionally, a nominal performance (NP) $H_{\infty}$ controller is designed. Closed-loop system is simulated with Orcad and simulation results of robust controller are compared with $H_{\infty}$ nominal performance controller. Although $H_{\infty}$ nominal performance controller has better performance for nominal plant, the robust performance controller is advantageous in dealing with uncertainties. 

Keywords: Robust control, Series Resonant Converter, Nominal Performance (NP), Robust Performance (RP).

1 Introduction

Nowadays power electronics converters are designed and manufactured with the emphasis on high power density, high efficiency, and low electromagnetic interface (EMI). To reduce the size of power supplies intended for use in modern equipment, it is desirable to increase the operating frequency to decrease the size of reactive components. Resonant converters are currently the object with prevalent interests among power conversion applications since high frequency operation with decreased switching losses can be achieved [1]-[3]. Control of switching power converters is necessary to regulate output voltage while robustly reject input variations in the presence of load and components uncertainties. Robust control theory allows the design of stabilizing controllers for plants that contain uncertainties.

In [4] a robust controller is designed for conventional variable frequency controlled SRC, where load variation was considered as unstructured uncertainty. Similar work on robust controller In [4] a robust controller is designed for conventional variable frequency controlled SRC, where load variation was considered as unstructured uncertainty. Similar work on robust controller design for parallel resonant converter is reported in [5]. In contrast, structured uncertainty is used in [6] to account for load variation in a duty-cycle controlled SRC. These controllers ignore the uncertainties arising from power circuit component tolerances. Robust controller design for a one-cycle controlled full-bridge series-parallel resonant inverter is proposed in [7]. This controller achieves robust stability and NP using “hinfsyn” function in MATLAB.

This paper presents an $H_{\infty}$ NP controller as well as a robust performance controller (RP) for SRC shown in Fig. 1. NP controller is designed using “hinfsyn” while “dksyn” is used to synthesize RP controller. For RP controller load uncertainty and power stage components uncertainties are taken into account using structured and unstructured uncertainty modeling, respectively. The $\mu$ synthesis approach described in [9] is used here for RP controller design.

2 Robust Control Problem

The well-established robust control theories are based mostly on linear time invariant (LTI) models. To design the controller, it is therefore more desirable to use, instead of the original time-varying switched model, a LTI model of the undergoing converter. Averaged modeling technique is proposed in [6], [8] to derive small-signal model of SRC, and is summarized here.

The equivalent circuit of SRC and applied tank voltage waveforms is illustrated in Fig. 2. The non-linear state-space equations of SRC can be written as

$$\frac{d \text{i}}{dt} = v_v - v - \text{sgn}(i) v_0$$

(1)
A slowly varying amplitude and phase transformation for the fast resonant state variables of SRC is defined as

\[ v(t) = u(t) \sin(\omega_0 t - \phi(t)) \]
\[ i(t) = C_0 u(t) \cos(\omega_0 t - \phi(t)) \]

First averaged model of SRC is obtained by averaging transformed equations over a switching period,

\[ \dot{v}_0 = \frac{2C_0 u \omega_0}{\pi C_f} \frac{G_v v_0}{C_f} - \frac{v_0}{C_f} \]
\[ \dot{u} = \frac{2\omega_0}{\pi \omega_0} \left( v_0 \sin \left( \frac{\pi d}{2} \right) \sin \phi - v_0 \right) \]
\[ \dot{\phi} = \frac{\omega_0^2 - \omega_0^2}{2\omega_0} + \frac{2v_0 \omega_0^2}{\pi \omega_0 u} \sin \left( \frac{\pi d}{2} \right) \cos \phi, \]

where \( \omega_0 \) is the angular resonant frequency defined as \( \omega_0 = \frac{1}{\sqrt{L C}} \), \( \omega_0 \) is the switching frequency, and \( d = D + \bar{d} \) is duty cycle. The perturbation and linearization of averaged model around the nominal operating point results in the following standard form for small-signal model of the converter,

\[ \dot{x} = Ax + B\hat{r} \]
\[ \hat{y} = Cx \]

where \( \dot{x} = [\dot{v}_0 \ \dot{u} \ \dot{\phi}] \), \( \hat{r} = [\dot{v}_0 \ \dot{i}_o \ \dot{v}_o] \), and \( \hat{y} = v_o \) denote state vector, input vector, and output, respectively. A, B, and C are given by the following expressions,

\[ A = \begin{bmatrix} \frac{G_v}{C_f} & \frac{2C_0}{\pi C_f} & 0 \\ \frac{2\omega_0^2}{\pi \omega_0} & 0 & \frac{2V_0 \omega_0^2}{\pi \omega_0} \sin \left( \frac{\pi}{2} \right) D \cos \phi \\ 0 & \frac{2V_0 \omega_0^2}{\pi \omega_0} \sin \left( \frac{\pi}{2} \right) D \sin \phi & \frac{1}{C_f} \end{bmatrix} \]

\[ B = \begin{bmatrix} \frac{2\omega_0^2}{\pi \omega_0} \left( \frac{2D}{\pi} \cos \phi \right) & \frac{V_0 \omega_0^2}{\omega_0} \cos \left( \frac{\pi D}{2} \right) D \sin \phi \\ \frac{2\omega_0^2}{\pi \omega_0} \left( \frac{2D}{\pi} \cos \phi \right) & \frac{V_0 \omega_0^2}{\omega_0} \cos \left( \frac{\pi D}{2} \right) D \sin \phi \\ 0 & 0 & \frac{1}{C_f} \end{bmatrix} \]

\[ C = \begin{bmatrix} 1 & 0 & 0 \end{bmatrix} \]

3 Nominal Performance Controller

A NP controller is designed to achieve following objectives,

1) Tracking, regulate output voltage to track reference signal.
2) Line regulation, the line voltage is often unregulated and could vary over a substantial range. This variation is modeled as an external disturbance, then leading to a disturbance rejection problem.

Load regulation, the load resistance could also vary over a wide range. For NP controller design, load variation is treated as external disturbance, too.

Modified control system block diagram for NP controller design is depicted in Fig. 3. The parameters for controller design are taken from [6], and are displayed in Table 1.
Table 1 Specification of SRC for controller design and simulation

<table>
<thead>
<tr>
<th>Parameter</th>
<th>Value</th>
</tr>
</thead>
<tbody>
<tr>
<td>Tank inductor $L$</td>
<td>285 $\mu$H</td>
</tr>
<tr>
<td>Tank capacitor $C$</td>
<td>10 nF</td>
</tr>
<tr>
<td>Filter capacitor $C_f$</td>
<td>33 $\mu$F</td>
</tr>
<tr>
<td>Input voltage $V_i$</td>
<td>10 V</td>
</tr>
<tr>
<td>Output voltage $V_o$</td>
<td>5 V</td>
</tr>
<tr>
<td>Switching frequency $f_s$</td>
<td>84.85 kHz</td>
</tr>
<tr>
<td>PWM gain $B$</td>
<td>1/9</td>
</tr>
<tr>
<td>Duty cycle $D$</td>
<td>0.62</td>
</tr>
<tr>
<td>Load resistance $R$</td>
<td>20-70 $\Omega$</td>
</tr>
</tbody>
</table>

4 Robust Performance Controller

4.1 Controller Design

A RP controller is designed to achieve tracking, line regulation, and load regulation considering following uncertainties in load and power stage components,

1) Load can vary over a wide range from 20 to 70 $\Omega$,
2) Inductors and capacitors are assumed to have a tolerance of 10%.

Load variation is modeled as structured uncertainty [6]. The load resistance can be expressed as an admittance form,

$$G_{\omega} = G_0 + \Delta G = G_0 + W \Delta,$$

where $G_0 = 1/3$ and uncertainty weighting function $W = 1/20 - 1/31 = 0.01824$ is used to obtain a normalized perturbation matrix with $||A||_\infty < 1$.

The unstructured uncertainty analysis is used to obtain a simple uncertainty model with the use of a full complex perturbation matrix $\Delta$, where at each frequency, $\Delta(j\omega)$ satisfying $\Delta(j\omega) \leq 1$. For a single-input single-output system, (15) gives the multiplicative uncertainty bound, where $G_{\omega \omega}$ and $W$ represent the perturbed plant, nominal plant, and multiplicative uncertainty bounds, respectively. Thus, any members of satisfy (16)

$$g_{\omega \omega} = \frac{G_{\omega \omega} - G_{\omega \omega}}{G_{\omega \omega}} < ||W||_\infty$$

$$G_{\omega \omega} = G_{\omega \omega}(1 + \Delta W), ||A||_\infty < 1$$

The difference function parameterizes the discrepancy between the nominal plant and the perturbation behavior of a real system. The uncertainties of the nominal plant model and disturbance dynamics model are analyzed in MATLAB. Fig. 7 shows the relative uncertainties of the nominal plant line to output transfer function $G_{\omega \omega}$ and disturbance plant with power circuit parameter variation. The relationship between the relative uncertainties and the plants component tolerances for $G_{\omega \omega}$ and $Z_o$ is plotted in Figs. 8 and 9.

From the uncertainty analysis, the multiplicative input uncertainty weighting function can be found using functions such as “lft2uss”. Functions $W_1$, $W_2$, and $W_3$ are given in Eqs. (17)-(19) as the multiplicative input uncertainty weighting function for $G_{\omega \omega}$, $G_{\omega \omega}$, and $Z_o$, respectively. A simple second order weighting function is used to keep the shape of the nominal plant’s variation.

$$W_1 = \frac{0.09572s^2 + 209s + 9.924 \times 10^4}{s^2 + 2709s + 1.557 \times 10^6}$$

$$W_2 = \frac{0.09856s^2 + 218.1s + 1.048 \times 10^5}{s^2 + 2736s + 1.596 \times 10^6}$$

$$W_3 = \frac{9.426 \times 10^{-6}s^2 + 117.2s + 8.427 \times 10^4}{s^2 + 635.9s + 1.081 \times 10^5}$$
**Fig. 4** Output voltage waveform for step change in the reference

**Fig. 5** Output voltage waveform for load step change (from 60 $\Omega$ to 31 $\Omega$)

**Fig. 6** Output response for step change in line voltage, (a) Input line voltage, (b) Output voltage for nominal plant, (c) Perturbed plant with 10.8 nF
The block diagram of RP controller synthesis is depicted in Fig. 10. The generalized system, P is given by

\[
P = \begin{bmatrix}
0 & 0 & 0 & 0 & W_1 & 0 \\
0 & 0 & 0 & 0 & 0 & W_2 B \\
W_2 G_d & W_2 G_v & W_2 Z_v & W_2 Z_o & 0 & W_2 G_m \\
-F_1 G_d & -F_1 G_v & -F_1 Z_v & -F_1 Z_o & F_1 & -F_1 G_m \\
-F_2 G_d & -F_2 G_v & -F_2 Z_v & -F_2 Z_o & F_2 & -F_2 G_m \\
-G_v & 0 & 0 & 0 & 0 & 0 & G_m B
\end{bmatrix}
\]

(20)

Uncertainty matrix has the following structure

\[
\Delta = \begin{bmatrix}
\Delta_{uv} & 0 \\
0 & \Delta_{pert}
\end{bmatrix}
\]

(21)

where \(\Delta_{pert}\) is a 2×2 full complex perturbation matrix, and \(\Delta_{uv}\) has the following block-diagonal structure

\[
\Delta_{uv} = \begin{bmatrix}
\Delta_1 & 0 & 0 & 0 \\
0 & \Delta_2 & 0 & 0 \\
0 & 0 & \Delta_3 & 0 \\
0 & 0 & 0 & \Delta_4
\end{bmatrix}
\]

(22)

The function “dksyn” in MATLAB is used to synthesize a robust controller via D-K iteration with performance weighting functions of (11), (12). After ten iterations a 12th order controller is obtained. Applying hankel-norm base approach for model reduction, a 3rd order transfer function is obtained

\[
K(s) = \frac{9.572 \times 10^7 s^2 + 1.153 \times 10^7 s + 2.041 \times 10^7}{s^3 + 3.646 \times 10^7 s + 5.984 \times 10^7 s + 5.623 \times 10^7}
\]

(23)

Fig. 11 shows framework for controller analysis. The closed-loop system has RP if and only if \(\mu(M) \leq 1\). In addition, closed-loop system is robustly stable if and only if \(\mu_{\Delta uv}(M_{11}) \leq 1\). From Figs. 12 and 13, it is apparent that closed-loop system has both robust stability and RP.

4.2 Simulation and Comparison

The RP controller of Eq. (17) is realized using op-amps and closed-loop system simulation results are displayed in Figs. 14 to 16. Fig. 14 shows that RP controller has primary objectives of tracking, line regulation, and load regulation for nominal plant. Output voltage waveform for a step change in the input voltage is shown Fig. 15 for several perturbations. Input voltage waveform is again the same as Fig. 6(a). It can be seen that the performance of the system is not affected by variation of the load resistance or power circuit components tolerances.

Output voltage waveform for a load step change (from 60 \(\Omega\) to 31 \(\Omega\)) is shown Fig. 16 for several perturbations. It is observed that power circuit components tolerances do not affect system performance significantly.

5 Conclusion

A \(NP\ H_{\infty}\) controller and a RP controller design for SRC were investigated in this paper. Both controllers have tracking, line regulation, and load regulation for nominal plant. RP controller is advantageous over \(NP\) controller in dealing with uncertainties. The RP controller achieves both robust stability and RP in the presence of load variation and power circuit components tolerances.
Fig. 10 RP controller synthesis  (a) Standard configuration  (b) SRC control system

Fig. 11 Analysis framework

Fig. 12 $\mu_\delta(M)$ to verify robust performance

Fig. 13 Robust stability
Fig. 14 Robust controller simulation results for nominal plant  
(a) Tracking  (b) Line regulation  (c) Load regulation
Fig. 15 Perturbed plant Output response for step change in line voltage

(a) $L = 300\mu H$  
(b) $C = 10.8nF$  
(c) $R = 70\Omega$
(d) $R = 50\Omega$  
(e) $C_f = 30\mu F$
References


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